

2 **Low-voltage ferroelectric–paraelectric superlattices as gate**  
3 **materials for field-effect transistors**

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7 **Abstract** The demand for new materials to be used in  
8 field-effect transistors and similar devices with low energy  
9 loss is more than ever before as integrated circuits have  
10 become a considerable source of energy consumption. One  
11 of the challenges in designing such energy efficient logic  
12 devices is finding suitable dielectric materials systems for  
13 the gate that controls the drain current in a *p*-type channel.  
14 A fundamental limit for energy efficiency exists in such  
15 devices imposed by the polarizability of conventional linear  
16 gate dielectrics. Generating on/off states in the channel  
17 that differ by at least a million times in the magnitude of  
18 the drain current near saturation requires several volts of  
19 gate bias for the case of a linear dielectric material in a  
20 submicron device. In this study, we demonstrate that ferroelectric–paraelectric superlattice heterostructures can generate the same effect in a *p*-type channel for bias voltages much lower than in a linear high dielectric constant gate. We consider a metal/superlattice/*p*-type semiconductor stack for this purpose. Using a thermodynamic model, we show that the multi-domain state of the ferroelectric layers can be tailored and distinct on/off states of the channel are possible for gate bias voltages below 1 V. The origins of such functionality of ferroelectric–paraelectric superlattices are discussed with respect to material

characteristics such as the phase transition temperature of 31  
the ferroelectric, total polarization, and the dielectric 32  
response. 33

**Introduction** 34

Integration of materials with unusual properties into elec- 35  
tronic devices paves the way for further developments and 36  
new functionalities. Such a trend has certainly been taking 37  
place in logic devices [1–3] such as the field-effect and 38  
metal–oxide–semiconductor transistors (FET and MOS- 39  
FET, respectively), where control of current in a semi- 40  
conductor (SC) channel through a gate is the main principle 41  
of operation. In particular, ever shrinking device dimen- 42  
sions have led to the search for new materials and multi- 43  
layer heterostructures that enable faster operation, lower 44  
leakage currents between the gate and the channel. More- 45  
over, the recent demand for low power consumption pre- 46  
sents an additional challenge in designing such devices. 47

Use of ferroelectric (FE) oxides as gate materials to 48  
induce on/off states in the channel of a FET type device has 49  
attracted significant interest since FEs possess a switchable 50  
remnant polarization. Switching the polarization direction 51  
via the gate bias can induce on/off states in the channel 52  
corresponding to significant differences in carrier densities 53  
between the two states, an outcome desired in a binary 54  
logic device not operating at ultra-high frequencies. 55  
Another motivation behind exploring FE-gated FETs [4– 56  
13] is that the electric field switchable remnant polarization 57  
could potentially be used as an additional functionality to 58  
store data, thus enabling, for example, a non-volatile gate 59  
memory. While FEs are certainly viable candidates to 60  
replace linear dielectrics in such devices, the sensitivity of 61  
functional properties of FEs to residual strains, interfaces, 62

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63 defects and electrostatic boundary conditions (BCs) are  
64 well known and must be taken into account [14–26]. For  
65 FE systems to become alternatives to current materials  
66 employed in FET/MOSFET, materials properties from a  
67 FE layer need to be comparable, if not better, than what is  
68 presently employed in device applications.

69 The polarization response, the dielectric constant, and  
70 electromechanical properties of FE are strongly tempera-  
71 **AQ2**ture dependent. Regardless whether the paraelectric (PE)–  
72 FE phase transformation is first- or second-order, there is  
73 an anomaly in the property coefficients near the PE–FE  
74 transformation at the Curie temperature  $T_C$ . The FE is more  
75 polarizable (or permeable and “soft”) when  $T_C$  is close to  
76 the operating (ambient) temperature compared to being  
77 “harder” if the ambient temperature is much lower than  
78  $T_C$ . High dielectric constants are thus possible in the  
79 vicinity of  $T_C$ , leading to efforts to target this temperature  
80 regime to enhance second-order property coefficients for a  
81 wide spectrum of applications.  $T_C$  of a FE oxide can be  
82 adjusted via controlling the strain state of the structure (for  
83 instance, by means of the choice of the substrate) [27–30]  
84 or judicious doping/alloying of the FE [31, 32].

85 Another unique way to control  $T_C$  is by growing alter-  
86 **AQ3**nating layers of FE and PE materials [33, 34]. These  
87 superlattices typically consist of ultra-thin repeating units  
88 of FEs and PEs, usually not exceeding 20 nm per layer.  
89 The idea is that stacking FEs with PEs or linear dielectrics  
90 might generate interface-driven interactions. Very high  
91 dielectric responses from such structures have already been  
92 reported [35–43]. In addition, there are other unexpected  
93 properties [16, 44–50] such as the demonstration of the  
94 formation of interfacial layers that behave different than  
95 the “bulk” (midsection) of the layers with reduced  
96 tetragonality [46], appearance of ferroelectricity in para-  
97 electric layers due to internal strain and electrical fields  
98 [51, 52], and the disappearance of the dielectric anomaly at  
99 the FE transition [69]. It is now well understood that it is  
100 the periodic contact between FE and PE layers that gener-  
101 ates internal electric fields opposing the FE polarization,  
102 and therefore, reducing the  $T_C$  of the structure with respect  
103 to the ideal metal/FE/metal case. That the FE layer tries to  
104 cope with the internal fields via formation of electrical  
105 domains is another phenomenon behind various interesting  
106 observations and predictions on these systems [46, 53–55].

107 Overall, the presence of a potentially very high dielec-  
108 tric response from a FE/PE superlattice stack and that this  
109 response can be controlled with small bias values ( $<1$  V)  
110 opens up the possibility to employ these structures as the  
111 gate in FET type devices. We note that such interface  
112 reactions have resulted in significant developments in  
113 magnetic multilayers and paved the way for new genera-  
114 tion of devices based on the giant magneto-resistance in  
115 ferromagnetic/metal/ferromagnetic hetero-layers [56]. In

116 this study, we analyze the characteristics and properties of  
117 a FE/PE superlattice-semiconductor interface and mecha-  
118 nisms by which a FE/PE superlattice stack can alter carrier  
119 distribution in a  $p$ -type semiconductor (pSC) similar to that  
120 of a channel in a FET or MOSFET. We use non-linear  
121 thermodynamics based on Landau–Ginzburg–Devonshire  
122 (LGD) theory and couple this with relevant Maxwell  
123 **AQ4** equations for dielectric solids to compute the polarization  
124 in the superlattice. By combining these results with Fermi–  
125 Dirac distribution of charged carriers and ionized dopants  
126 in the superlattice and SC, we show that effective carrier  
127 control can be achieved with gate bias values much lower  
128 than those for an ordinary linear dielectric material. The  
129 multi-domain (MD) state of the FE/PE structure that may  
130 form due to depolarizing fields in the FE layers is the key  
131 to form a discontinuous or a continuous carrier gas at the  
132 superlattice/pSC interface leading to insulating-to-con-  
133 ducting transitions of the channel. The system that we  
134 investigate in detail in this study is a  $\text{PbZr}_{0.3}\text{Ti}_{0.7}\text{O}_3/\text{SrTiO}_3$ ·(PZT/STO)·FE/PE superlattice heterostructure  
135 sandwiched between pSC and Pt electrodes. PZT/STO is  
136 specifically chosen because of the relatively low misfit  
137 between PZT and STO ( $\sim 1\%$  at room temperature, RT).  
138 We calculate electrical domain configurations based on the  
139 number of repeating PZT–STO units and provide numeri-  
140 cal results of the overall polarization as a function of  
141 temperature and the charge concentration variation with  
142 gate voltage. Our results demonstrate clearly that such  
143 multilayer heterostructures have indeed the potential to be  
144 employed as gate oxides in FETs and/or MOSFETs. 145

## 146 Theoretical approach

147 A schematic drawing of the PZT/STO superlattice system  
148 considered in our model is given in Fig. 1. We specifically  
149 study equi-thickness PZT/STO systems although such a  
150 restriction can be relatively easily relaxed [57]. As defined  
151 in Fig. 1,  $\lambda$  is the thickness of the repeating unit,  $n$  is the  
152 number of repeating units,  $d$  is the thickness of the metal  
153 and the SC layer, and  $L$  is the total thickness of the  
154 superlattice. The stacks are taken as being infinite along the  
155  $y$ -direction, reducing the problem to two dimensions. We  
156 assume that all layers are grown pseudomorphically onto a  
157 (001) STO substrate and the system is short-circuited. The  
158 SC bottom electrode, namely the channel, is heavily  $p$ -  
159 doped with shallow acceptor dopants at a concentration of  
160  $10^{24} \text{ m}^{-3}$  with each acceptor atom receiving one electron  
161 from the valence band and is grounded at all times, while  
162 the superlattice constituents are considered to be intrinsic  
163 wide band gap layers. The semiconducting parameters of  
164 the pSC, FE, and PE layers are provided in Table 1 [32,  
165 58–60].

166 Maxwell equations as applied to the FE/PE superlattice  
 167 and the pSC layer are satisfied such that:

$$\nabla \cdot \mathbf{D} = \rho \tag{1}$$

169 and we can express dielectric displacement vector as:

$$\mathbf{D} = (D_x, 0, D_z) \tag{2}$$

171 where

$$D_x = \epsilon_0 \epsilon_b E_x + P_x \text{ and } D_z = \epsilon_0 \epsilon_b E_z + P_z \tag{3}$$

173 in the FE/PE with  $x$  and  $z$  denoting the in-plane and out-of-  
 174 plane components respectively and,

$$D_x = \epsilon_0 \epsilon_r E_x \text{ and } D_z = \epsilon_0 \epsilon_r E_z \tag{4}$$

176 in the pSC that has a dielectric constant of  $\epsilon_r$ . The top  
 177 metal is assumed to behave as an ideal metal and no  
 178 electric field can penetrate it (meaning the screening length  
 179 is unphysically thin) but its potential can be controlled  
 180 externally. In Eqs. 3 and 4,  $\epsilon_0$  is the permittivity of vacuum  
 181 and  $\epsilon_b$  is the background dielectric constant (taken as seven  
 182 here [61, 62]) of the FE/PE (same value in both layers),  $E_x$   
 183 and  $E_z$  are components of the electric field vector  $\mathbf{E} = (E_x,$

184  $0, E_z)$  which follow from  $E_x = -\partial\phi/\partial x$  and  $E_z = -\partial\phi/\partial z$   
 185 and, and  $P_x$  and  $P_z$  are the components of the polarization  
 186 vector  $\mathbf{P} = (P_x, 0, P_z)$ .  $\rho$  is the total charge density and  
 187 consists of electrons and holes in the FE/PE, pSC in  
 188 addition to ionized acceptors that are present only in the  
 189 pSC channel:

$$\rho = q(-n^- + p^+ - N_A^-) \tag{5}$$

where

$$N_A^- = N_A \left( \exp\left(\frac{q(E_A - E_F - \phi)}{kT}\right) + 1 \right)^{-1} \tag{6a}$$

$$n^- = N_C \left( \exp\left(\frac{q(E_C - E_F - \phi)}{kT}\right) + 1 \right)^{-1} \tag{6b}$$

$$p^+ = N_V \left[ 1 - \left( \exp\left(\frac{q(E_V - E_F - \phi)}{kT}\right) + 1 \right)^{-1} \right] \tag{6c}$$

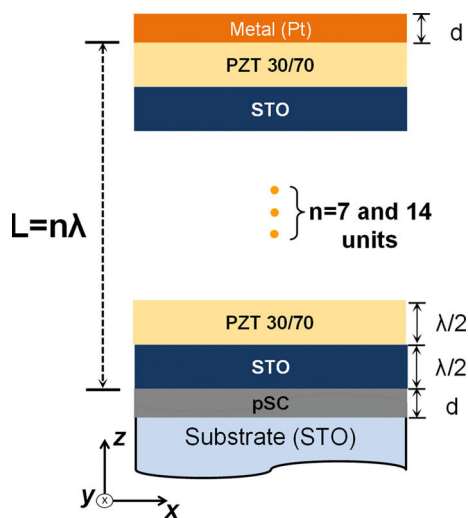
197  $N_A^-$  is the ionized acceptor density in the pSC,  $n^-$  is the  
 198 electron density at any given coordinate except the top  
 199 metal electrode,  $p^+$  is the hole density,  $N_C$  is the effective  
 200 density of states at the bottom of the conduction band and  
 201  $N_V$  is the effective density of states at the top of the valence  
 202 band of a given layer (except the top metal),  $E_C$  is the  
 203 energy of an electron at the bottom of the conduction band,  
 204  $E_V$  is the energy of an electron at the top of the valence  
 205 band,  $E_F$  is the Fermi level,  $\phi$  is the local electrostatic  
 206 potential and  $E_A$  is the ionization energy of the acceptor  
 207 atom that is taken with respect to the top of the valence  
 208 band,  $k$  is the Boltzmann constant in eV units, and  $T$  is  
 209 temperature in Kelvin. To carry out the calculations  
 210 including the band bending in the FE/PE stack, one needs  
 211 to know  $E_F$  of the metal/FE/PE/pSC structure which is  
 212 taken to be that of Pt as the stack will equilibrate with the  
 213 Fermi level of Pt upon contact.

214 The electrostatic BCs for the potential are needed to  
 215 obtain solutions to the Eqs. 1–6. The BCs for the electro-  
 216 static potential along the thickness of the superlattice is:

$$\phi_{FE} = \phi_{pSC} \text{ for } z = n\lambda/2, \tag{7}$$

218 where  $n$  is an integer denoting a PE/FE interface and Eq. 7  
 219 ensures the continuity of the potential at each interface and

$$\phi_{metal} = \phi_{pSC} = 0 \text{ for } z = 0, L \tag{8}$$



**Fig. 1** A schematic drawing of the superlattice for which the  
 computations are carried out.  $\lambda$  and  $d$  are the thickness of the  
 repeating unit and Pt or pSC, respectively.  $n$  is the number of  
 repeating units and  $L$  is the total thickness of the metal/FE/PE/pSC  
 heterostructure on STO

**Table 1** Band parameters, ionization energies of dopants and linear dielectric values the pSC, nSC, and the FE used in the calculations

	$E_F$ (eV)	$N_C$ ( $m^{-3} E^{-1}$ )	$N_V$ ( $m^{-3} E^{-1}$ )	$N_A$ ( $m^{-3}$ )	$E_A, E_D$ (eV)	$E_C, E_V$ (eV)	$\epsilon_r$ ( $\epsilon_b$ in FE)
pSC	-5.1	$10^{25}$	$10^{25}$	$10^{24}$	-0.05	-4.05, -5.15	10
FE	-5.7	$10^{24}$	$10^{24}$	none	none	-4.2, -7.4	7
PE	-5.4	$10^{24}$	$10^{24}$	none	none	-3.9, 7.1	7

$m^{-3} E^{-1}$  is the unit for density of states ( $E$  energy unit, eV)

for short circuiting conditions where we assumed the Pt top metal electrode behaves ideal (the electric field does not penetrate into the electrode) and the bottom pSC/Pt electrode is ideal as well. When a bias is applied to the system, potential in the top metal is raised or lowered depending on the sign of the bias with respect to the other end of the stack, i.e., the bottom electrode, which is electrically grounded at all times. Note that, before considering any external bias effects, the condition of equality of electrochemical potential causing charge transfer between the layers automatically imposes the presence of a built-in field in the FE/PE superlattice and a position-dependent depletion charge distribution as a consequence. The electric field in the FE/PE superlattice satisfies the LGD equations of state given as:

$$w \left\langle \begin{aligned} &2\alpha_3^m P_z + 4\alpha_{13}^m P_z P_x^2 + 4\alpha_{33}^m P_z^3 + 6\alpha_{111} P_z^5 \\ &+ \alpha_{112} (4P_z P_x^4 + 8P_z^3 P_x^2) + 2\alpha_{123} P_z P_x^4 - \gamma \left( \frac{\partial^2 P_z}{\partial z^2} + \frac{\partial^2 P_z}{\partial x^2} \right) \end{aligned} \right\rangle_{FE} \\ + (1-w) \left\langle \begin{aligned} &2\alpha_3^m P_z + 4\alpha_{13}^m P_z P_x^2 + 4\alpha_{33}^m P_z^3 - \gamma \left( \frac{\partial^2 P_z}{\partial z^2} + \frac{\partial^2 P_z}{\partial x^2} \right) \end{aligned} \right\rangle_{PE} \\ = wE_z + (1-w)E_z \tag{9a}$$

$$w \left\langle \begin{aligned} &2\alpha_1^m P_x + 2(2\alpha_{11}^m + \alpha_{12}^m) P_x^3 + 2\alpha_{13}^m P_x P_z^2 + 6\alpha_{111} P_x^5 \\ &+ 2\alpha_{112} [3P_x^5 + 3P_x^3 P_z^2 + P_x P_z^4] + 2\alpha_{123} P_x^3 P_z^2 - \gamma \left( \frac{\partial^2 P_x}{\partial z^2} + \frac{\partial^2 P_x}{\partial x^2} \right) \end{aligned} \right\rangle_{FE} \\ + (1-w) \left\langle \begin{aligned} &2\alpha_1^m P_x + 2(2\alpha_{11}^m + \alpha_{12}^m) P_x^3 + 2\alpha_{13}^m P_x P_z^2 - \gamma \left( \frac{\partial^2 P_x}{\partial z^2} + \frac{\partial^2 P_x}{\partial x^2} \right) \end{aligned} \right\rangle_{PE} \\ = wE_x + (1-w)E_x \tag{9b}$$

Here,  $w$  is an arbitrary function we introduce to assign the coordinates of the FE/PE interfaces and the repeating unit thickness of the superlattice ( $\lambda$ ) and determine the total superlattice thickness.  $w$  is valid only in the superlattice as defined below:

$$\Omega = \text{sgn}(\sin \frac{2\pi z}{\lambda}), \tag{10}$$

where  $z$  is thickness from the bottom pSC/superlattice interface to the top superlattice/metal interface (Fig. 1). Using the values of  $\Omega$  we choose:

$$\text{FE layer} \rightarrow \text{if } \Omega > 0, \text{ PE layer} \rightarrow \text{if } \Omega < 0, \tag{11a}$$

and therefore

$$w = 1 \text{ if } \Omega > 0 \text{ and } w = 0 \text{ otherwise.} \tag{11b}$$

In Eqs. 9a and 9b;  $\alpha_1^m, \alpha_3^m, \alpha_{11}^m, \alpha_{33}^m, \alpha_{12}^m,$  and  $\alpha_{13}^m$  are the renormalized dielectric stiffness coefficients in SI units given by:

$$\alpha_1^m = \alpha_1 - u_m \frac{2(Q_{11} + Q_{12})}{s_{11} + s_{12}}, \alpha_3^m = \alpha_1 - u_m \frac{4Q_{12}}{s_{11} + s_{12}}, \tag{12a}$$

$$\alpha_{11}^m = \alpha_{11} + \frac{2}{s_{11}^2 - s_{12}^2} [(Q_{11}^2 + Q_{12}^2)s_{11} - 2Q_{11}Q_{12}s_{12}], \tag{12b}$$

$$\alpha_{33}^m = \alpha_{11} + \frac{4Q_{12}^2}{s_{11} + s_{12}}, \tag{12c}$$

$$\alpha_{12}^m = \alpha_{12} - \frac{2}{s_{11}^2 - s_{12}^2} [(Q_{11}^2 + Q_{12}^2)s_{12} - 2Q_{11}Q_{12}s_{11}] + \frac{Q_{44}^2}{s_{44}}, \tag{12c}$$

$$\alpha_{13}^m = \alpha_{12} + \frac{2Q_{12}(Q_{11} + Q_{12})}{s_{11} + s_{12}}, \tag{12c}$$

where  $\alpha = (2\epsilon_0 C)^{-1}$ ,  $Q_{ij}$  and  $S_{ij}$  are electrostrictive coefficients and components of the elastic stiffnesses at constant polarization, respectively, and  $\alpha_i, \alpha_{ij}$ , and  $\alpha_{ijk}$  are the dielectric stiffness coefficients of bulk PZT. We note that  $\alpha_{12}^m$  and  $\alpha_{33}^m$  contain the clamping effect of the film,  $\gamma$  is the gradient energy coefficient and is assumed to be isotropic for convenience and is taken to be  $6 \times 10^{-10} \text{ m}^3 \text{ F}^{-1}$  [63]. The thermodynamic, elastic, and electromechanical data used in the calculations are given in Table 2 [32, 59, 60].

The pseudo-cubic (polarization-free) misfit strain tensor in PZT is defined as:

**Table 2** Bulk thermodynamic, elastic, and electromechanical coefficients of PZT 30/70 and STO

	PZT 30/70	STO
$a$ (nm)	0.3950	0.3904
$T_C$ (°C)	440.2	-253
$C$ ( $10^5$ °C)	1.881	0.8
$Q_{11}$ ( $\text{m}^4 \text{ C}^{-2}$ )	0.07887	0.0457
$Q_{12}$ ( $\text{m}^4 \text{ C}^{-2}$ )	-0.02480	-0.013
$Q_{44}$ ( $\text{m}^4 \text{ C}^{-2}$ )	0.06356	0.00957
$s_{11}$ ( $10^{-12} \text{ N m}^{-2}$ )	8.4	3.729
$s_{12}$ ( $10^{-12} \text{ N m}^{-2}$ )	-2.7	-0.9088
$s_{44}$ ( $10^{-12} \text{ N m}^{-2}$ )	17.5	
$\alpha_{11}$ ( $10^7 \text{ N m}^6 \text{ C}^{-4}$ )	0.6458	170
$\alpha_{12}$ ( $10^8 \text{ N m}^6 \text{ C}^{-4}$ )	5.109	27.4
$\alpha_{111}$ ( $10^8 \text{ N m}^{10} \text{ C}^{-6}$ )	2.348	-
$\alpha_{112}$ ( $10^8 \text{ N m}^{10} \text{ C}^{-6}$ )	10.25	-
$\alpha_{123}$ ( $10^9 \text{ N m}^{10} \text{ C}^{-6}$ )	-5.003	-
$\gamma$ ( $10^{-10} \text{ m}^3 \text{ F}^{-1}$ )	6	6

$$u_{ij}^m = \begin{pmatrix} u_m & 0 & 0 \\ 0 & u_m & 0 \\ 0 & 0 & -2u_m S_{12}/(S_{12} + S_{11}) \end{pmatrix} \text{ with} \quad (13)$$

$$u_m = \frac{a_{\text{STO}} - a_{\text{PZT}}}{a_{\text{STO}}}$$

274 where  $u_m$  is the in-plane misfit strain which enters Eqs. 9a,  
 275 9b, and 12a,  $a_{\text{STO}}$  is the lattice parameter of the STO  
 276 substrate (Fig. 1) and  $a_{\text{PZT}}$  is the pseudo-cubic bulk lattice  
 277 parameter of PZT. Since all layers are assumed to be  
 278 pseudomorphic, the in-plane misfit  $u_m$  in STO layers in the  
 279 superlattice equals 0. The polarization-free misfit strain  $u_m$   
 280 in PZT is  $\sim 3\%$  at RT which corresponds to an actual  
 281 misfit of  $\sim 1\%$  which ensures that the FE polarization is  
 282 along the  $z$ -axis.

283 Periodic BCs are employed along the plane of the  
 284 structures for polarization and the electrostatic potential as  
 285 well. The polarization BCs at the FE/PE and metal/FE  
 286 interfaces can be expressed as:

$$\left[ P_z + \beta \frac{dP_z}{dz} \right]_{z=0,L} = 0, \quad (14a)$$

288 
$$\left[ P_x + \beta \frac{dP_x}{dz} \right]_{z=0,L} = 0 \quad (14b)$$

290 with  $z$  indicating the coordinates for metal/FE (top) and PE/  
 291 pSC (bottom,  $L = 0$ ) interfaces,  $\beta$  is the extrapolation  
 292 length describing the extent of change of  $P_z$  ( $P_x$ ) along  
 293 (perpendicular to) the film normal at the interface and is a  
 294 parameter describing how strongly ferroelectricity is sup-  
 295 pressed near the electrode interfaces (taken as 3 nm here  
 296 based on previous reports [61, 62]. We assume that the  
 297 interfaces of the FE and PE layers are “neutral” with  
 298 respect to the transition temperature of the interior of the  
 299 layers. This means that the surfaces of the FE and PE layers  
 300 are assumed to have the same  $T_C$  as bulk of the layers  
 301 ( $\beta \rightarrow \infty$ ). We do so to focus on the electrode interfaces as  
 302 small values of  $\beta$  can complicate the analysis of the results.  
 303 Furthermore, such an approach has yielded theoretical  
 304 results [64] in very good agreement with experimental  
 305 findings [65].

306 We employ a finite difference discretization in two  
 307 dimensions and carry out a Gauss–Seidel iterative scheme  
 308 to solve the coupled Eqs. 1, 4, 5, 11, and 14 simultaneously  
 309 subject to the BCs provided in Eqs. 11–14. The computa-  
 310 tion grid consists of  $m \times 200$  points where  $m$  is the number  
 311 of nodes along the thickness that vary depending on the  
 312 superlattice size considered (298 nodes for both the pSC  
 313 and the superlattice and 1 node for top/bottom metal to  
 314 specify the potential BCs, making a total of 300 nodes).  
 315 The node-to-node distances, namely  $h$ , are taken as 0.4 nm,  
 316 almost the unit cell size of the pseudo-cubic PZT and STO  
 317 and, therefore,  $mh = n\lambda$ . We terminate the iteration after

3000 loops that yield a difference of less than  $10^{-3} \text{ C m}^{-2}$  318  
 for polarization between two consecutive steps. To ensure 319  
 the correctness of the numerical solutions, we applied our 320  
 approach to test cases such as homogeneous FE ( $\beta \rightarrow \infty$ ) 321  
 with ideal electrodes and FE sandwiched between 2 PE 322  
 layers as in [64, 66] where we obtained excellent agree- 323  
 ment with analytical solutions (not shown here). 324

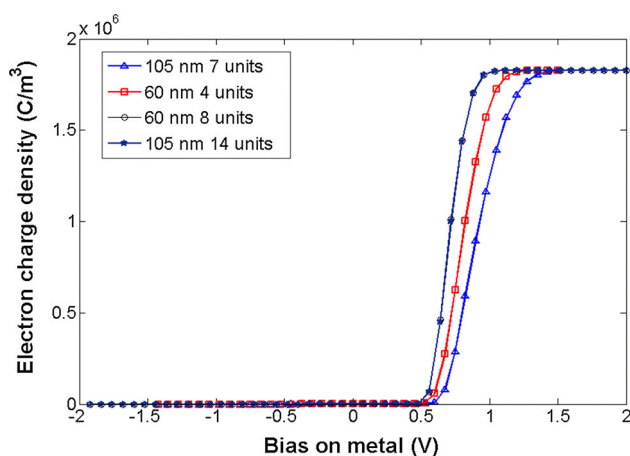
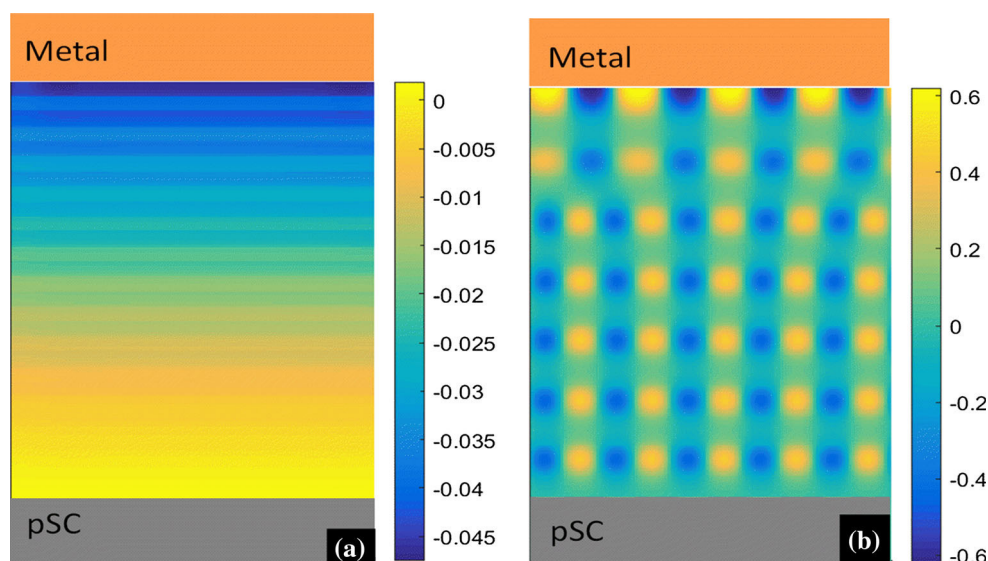
## Domain structures and transition temperatures of superlattices 325 326

327 We first focus on the effect of layer periodicity of the FE/  
 328 PE superlattices as this determines the FE/PE transition  
 329 temperature and potentially the bias enabling carrier den-  
 330 sity control. Anticipating that the carrier density at the  
 331 superlattice/pSC interface will be a function of domain  
 332 states and the magnitude of the (total) polarization, we start  
 333 off with the domain structures of two stacks having the  
 334 same total thickness of 105 nm but differing in number of  
 335 units, namely  $n = 7$  and 14 with repeating unit thicknesses  
 336  $\lambda = 15$  and 7.5 nm, respectively. Polarization maps at RT  
 337 are provided in Fig. 2. Each stack has the FE PZT layer as  
 338 the first layer in contact with the top metal electrode and  
 339 the structures both terminate with the PE STO layer. We  
 340 chose to terminate the stacks with STO as this material  
 341 provides a good barrier to leakage currents [67, 68] and has  
 342 exceptional polarizability that would potentially allow the  
 343 transmission of domain wall-related phenomena in the FE  
 344 layer to the pSC interface. We have also analyzed two  
 345 different thicknesses for each stack type as we would like  
 346 to reveal the field dependence of the carrier density  
 347 response at the superlattice/pSC interface. This, however,  
 348 did not result in discernible differences in the results for the  
 349 “take-off” bias, which is around 0.5 V, as shown in Fig. 3.  
 350 This is because the transition temperature and thus the  
 351 domain structure of the superlattice do not depend on the  
 352 total thickness of the heterostructure but rather on the  
 353 repeating unit thickness [66]. We note that the “take-off”  
 354 bias might not necessarily correspond to onset of conduc-  
 355 tion in the p-type channel as the discrete carrier concen-  
 356 trations need to merge to form a continuous carrier sheet  
 357 at the FE/pSC interface for the “on” state as we shall show in  
 358 the next section. All what is discussed until here will cer-  
 359 tainly not be the case if the bias is much larger than what is  
 360 used here to demonstrate channel control. Such high fields  
 361 and their effects are outside the scope of the present study.

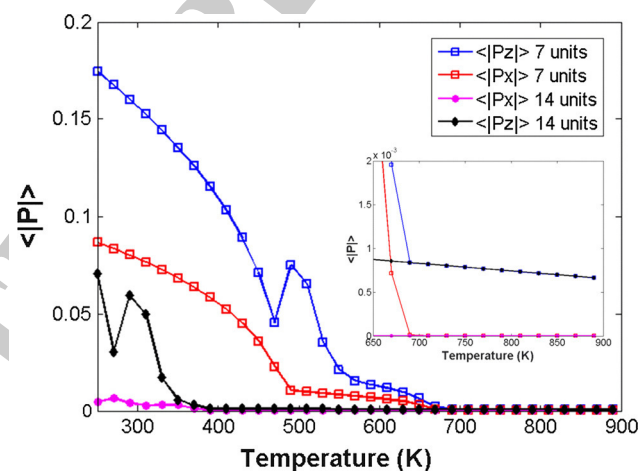
362 As such, we decided to focus on the domain states and  
 363 transition characteristics of the relatively thick (105 nm)  
 364 stacks. The 7-unit superlattice with metal top and bottom  
 365 pSC electrodes is in a distinct MD state, while the 14-unit  
 366 superlattice is either in a weak single domain (SD) or a  
 367 very wide domain periodicity MD regime, i.e., the domain

Author Proof

**Fig. 2** RT out-of-plane polarization maps for 105-nm-thick PZT/STO superlattices with **a**  $n = 14$  and **b**  $n = 7$  repeating units on STO. The units on the vertical scales are in  $C/m^2$ . The polarization in the superlattice with  $n = 14$  is considerably smaller than that of the superlattice with  $n = 7$  due to relatively larger build-in fields



**Fig. 3** Bias-dependent carrier density of PZT/STO superlattices as a function of  $n$  and  $L$ . The carrier density of the 60 nm stack with  $n = 8$  is identical to that of 105-nm stack with  $n = 14$



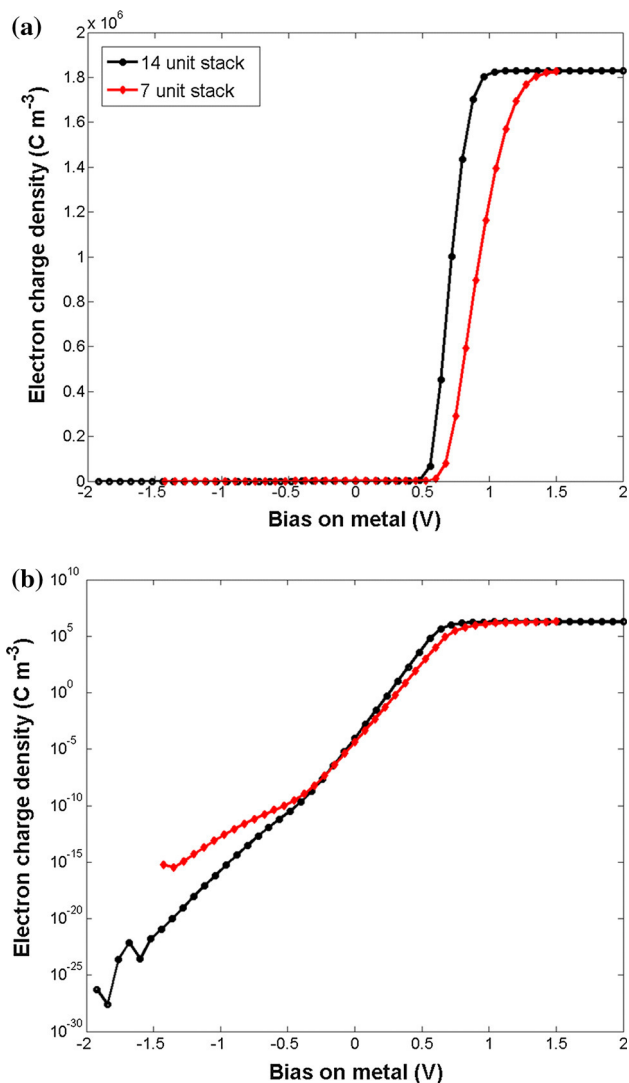
**Fig. 4** Temperature-dependent absolute average values of in-plane  $\langle |P_x| \rangle$  and out-of-plane polarizations  $\langle |P_z| \rangle$  for 105-nm-thick PZT/STO superlattices with  $n = 7$  and  $n = 14$  repeating units on STO. The inset shows small built-in polarization due to the top/bottom electrode asymmetry. Note that the  $P_z$  for 14- and 7-unit stacks almost completely overlap and are hard to distinguish due to their identical dielectric response far above their respective  $T_C$

368 size is larger than the lateral grid size in the computations.  
 369 It is almost certain that, in the light of prior experiments  
 370 and theoretical predictions on such systems [64–66], the  
 371 two stacks with different unit thicknesses will have dif-  
 372 ferent transition temperatures, which are computed and  
 373 plotted as shown in Fig. 4. The transition temperatures of  
 374 the two stacks can be found from investigating  $\langle |P_z| \rangle$  vs.  
 375 temperature where the departing point of  $\langle |P_z| \rangle$  from the  
 376 flat background polarization can be taken as the reference  
 377 state. The stack with smaller  $n$  (14 units) has a FE tran-  
 378 sition temperature that is considerably lower than that of  
 379 the stack with seven units. This also impacts the domain  
 380 stabilities of the two stacks in comparison: the 7-unit  
 381 stack is stabilized in the MD state while the 14-unit stack  
 382 is apparently in a weak-SD state, where the latter is  
 383 probably also favored by the asymmetry in top/bottom

384 interfaces. One should expect the stacks considered here  
 385 to behave differently from those similar structures ana-  
 386 lyzed in previous studies since these have considered  
 387 either ideal symmetrical top/bottom electrodes or infinite  
 388 systems (periodic BCs) along the film/heterostructure  
 389 thickness [64, 66, 69]. A small but finite built-in polar-  
 390 ization due to the top–bottom electrode asymmetry is  
 391 expected. This is indeed confirmed as shown in the inset  
 392 of Fig. 4. In the case of symmetric top/bottom electrodes,  
 393 no such built-in polarization exists as previously shown  
 394 in detail in Ref. [69] and our results converge to that of  
 395 shown in that paper.

396 **Carrier density at the superlattice/pSC interface**

397 The bias dependence of the carrier density near the  
 398 superlattice/pSC interface is plotted in Fig. 5. We provide  
 399 here the results for two stacks with different number of  
 400 repeating units. Quite significant carrier density differences  
 401 can be obtained at the superlattice/pSC interface within a  
 402 small range of bias on the top metal. Carrier density maps  
 403 for the 14 unit stack for two bias values of the top metal (0  
 404 and 0.8 V) are given in Fig. 6. There is about 11 orders of  
 405 magnitude difference in the carrier density at the FE/pSC  
 406 interface when stacks of 0 and 0.8 V are considered. This is  
 407 in addition to the fact that 0 V bias results in “discrete” or



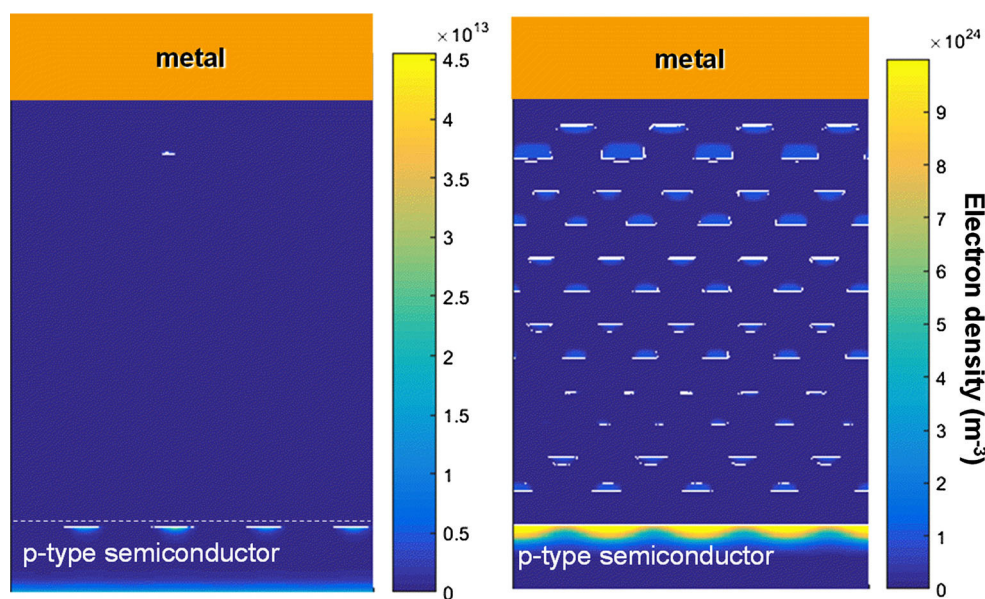
**Fig. 5** Gate bias dependence of the electron charge density near the pSC/PZT interface for a 120-nm-thick pSC/PZT/STO heterostructure with  $n = 7$  and 14 units. The same data are plotted on **a** linear and **b** logarithmic scales. The fluctuations of electron charge density at gate bias smaller than  $-1.25$  V are due to the fact that numerical approach computer precision is not of physical origin

“discontinuous” sheet-like carrier density compared to 408  
 0.8 V bias where there is a formation of a continuous film 409  
 of carriers. Curves similar to what is provided in Fig. 5 for 410  
 the positive gate voltages on the metal but for drain cur- 411  
 rents have been reported previously for other FE systems 412  
 such as single layer  $\text{SrBi}_2\text{Ta}_2\text{O}_9$  (SBT) [70]. Here, we are 413  
 able to analyze the shape of such curves in the relatively 414  
 simpler model systems in connection with the domain 415  
 states and the transition temperatures. 416

An important outcome of our results is the relatively low 417  
 bias values on the gate under which significant carrier 418  
 densities can form on the pSC side of the superlattice/pSC 419  
 interface. Particularly, the case of 14 units can reduce the 420  
 necessary gate voltage to induce significant variations in 421  
 pSC minority carrier densities, i.e., electrons, near the 422  
 interface. Having stated that the polarization magnitude of 423  
 the FE layers drives the accumulation of carriers, one also 424  
 needs to consider the ease with which the domain walls 425  
 move in response to an applied bias. The stack with the 426  
 lower  $T_C$  should be expected to be “softer,” i.e., should 427  
 have relatively higher domain wall mobility, leading to a 428  
 higher *effective* dielectric response. 429

It is clear from Eqs. 7, 8, 14 that polarization gradients 430  
 determine the local electrostatic potential. As such, this is a 431  
 non-linear problem, which makes it difficult to provide 432  
 quantitative solutions. Nonetheless, we can attempt to 433  
 analyze the amount of band bending near the FE/pSC 434  
 interface and comment on the different extents of carrier 435  
 accumulation near that interface in the two stacks to shed 436  
 light on the effect of  $T_C$  and thus the polarization strength. 437  
 In Figs. 7, 8, 9, we plot the flat-band energy diagrams that 438  
 are calculated by imposing the electrostatic potential on the 439  
 band energies of each materials system. We must point out 440  
 that results will differ for domains with polarization along 441  
 the positive and negative  $z$ -axis. Furthermore, electrical 442  
 BCs such as the presence or absence of a bias voltage at the 443  
 top electrode should affect the internal potential and, 444  
 therefore, the flat-band diagram. The zero bias band 445  
 bending, particularly in the seven unit stack, is reminiscent 446  
 of multilayers/superlattices of polar semiconductors such 447  
 as InN/GaN or GaN/AlN [71–73]. The difference here is 448  
 that the bending is due to the presence of a FE polarization 449  
 that is switchable (Fig. 7a) compared to the un-switchable 450  
 ionic plus piezoelectric polarization in compound polar 451  
 semiconductors. In the MD state, the bands in the positive 452  
 and negative domains will have opposite slopes. Applica- 453  
 tion of a positive bias to the top metal pulls down the 454  
 potential values, the STO layer becomes polarized, mini- 455  
 mizing the polarization mismatch at the interlayer inter- 456  
 faces. This causes the potential profile of the bands to 457  
 flatten as shown in the 7-unit stack (Fig. 7b). The zero bias 458  
 band profile is rather smooth in the 14 unit stack as the 459  
 polarization in the layers is almost constant due to a SD- 460

**Fig. 6** RT carrier density map of 120-nm-thick pSC/PZT/STO heterostructure for **a** 0 V and **b** 0.8 V bias. For the stack with 0.8 V bias, the carrier density at the pSC/FE interface is more than 11 orders of magnitude higher than the stack with 0 V bias

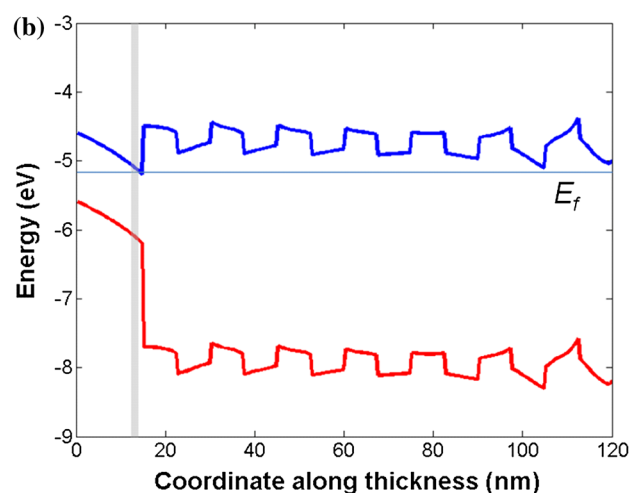
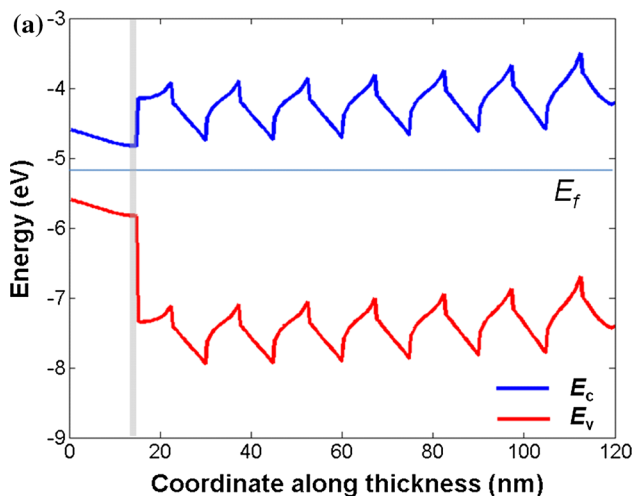


461 like state (Fig. 8a) and a polarization with low but almost  
 462 equal magnitude in the layers. A bias as small as 0.8 V can  
 463 shift the entire band structure due to an almost constant  
 464 polarization profile (please see Fig. 2a) owing to the high  
 465 polarizability of the STO layers and that the stack is not far  
 466 from  $T_C$ . A rather steep band bending, on the other hand,  
 467 occurs on the pSC side as the superlattice polarization  
 468 makes a jump whose bound charges can only be partially  
 469 screened by the pSC (Fig. 8b). Apparently, a constant but  
 470 small polarization termination near the superlattice/pSC  
 471 interface has a stronger influence on the band bending in  
 472 the pSC with respect to a MD state terminating at the same  
 473 interface where the latter has an alternating sign of  
 474 potential. Thus, the multilayer heterostructure with lower  
 475 Curie temperature is more susceptible to becoming a SD  
 476 state system, particularly in the presence of asymmetric  
 477 top/bottom interfaces, favoring the behavior in Fig. 4.  
 478 Keeping in mind that the slope of the band slope from the  
 479 pSC side will determine the electron accumulation, we  
 480 focus on the pSC/FE interfaces given in Fig. 8a, b. Indeed,  
 481 Fig. 9 reveals that the amount of band bending in the pSC  
 482 layer interfacing a 7-unit or a 14-unit stack is markedly  
 483 different. The band diagram of the 14-unit superlattice has  
 484 a relatively steeper slope and hence a higher accumulation  
 485 of carriers. Such an occurrence originates from the softness  
 486 of the polarization in the latter according to our results.  
 487 Therefore, one can expect that a wide domain structure, or  
 488 even a possibly weak-SD state near the transition temper-  
 489 ature to generate significant carrier density differences in  
 490 the pSC channel for on/off states owing to the suscepti-  
 491 bility of polarization to applied bias. One can eventually  
 492 expect that a SD state will lead to stronger band bending  
 493 than an MD state where the latter has an electrostatic

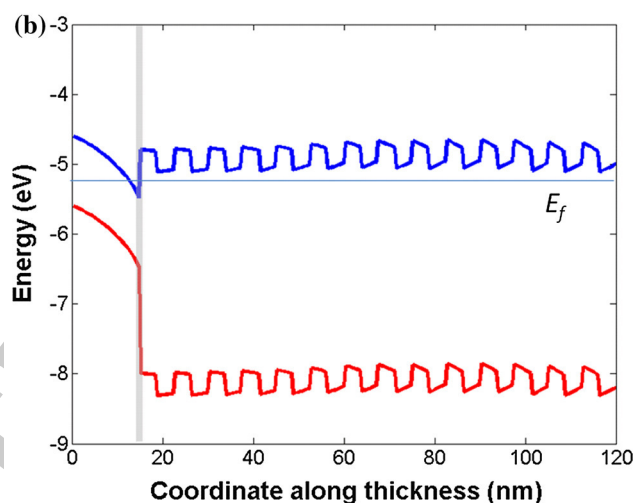
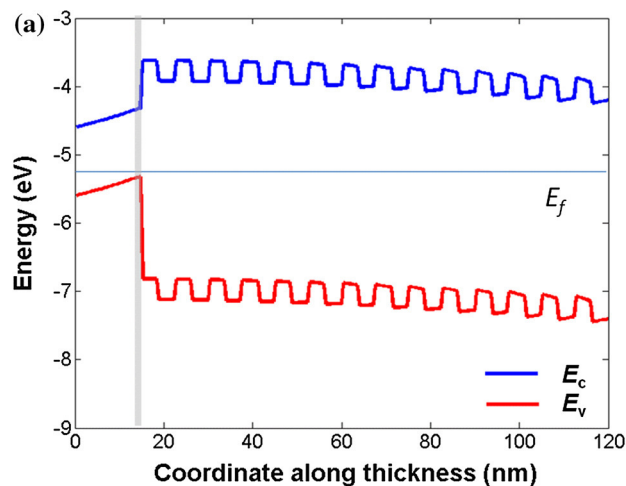
potential alternating in sign. Note that the temperature at  
 494 which  $P_z$  changes its slope due to the appearance of  $P_x$  is  
 495 almost equal to RT. High dielectric response in this regime was shown previously [69]. However, due to the highly non-linear dependence of the dielectric constant on applied field in such structures and considering their high sensitivity to electrode interfaces, we realize such reasoning requires further detailed analysis that we leave to a future study. While a FET or MOSFET-type device can benefit from a FE/PE superlattice gate for channel control at relatively low bias values relative to linear ordinary dielectrics, a wide MD or a weak-SD state in the superlattice, occurring when the ambient operation temperature is not far from  $T_C$ , leads to a higher domain wall mobility under smaller fields and can allow more effective control of carrier densities in the pSC channel.

## 510 Summary and outlook

511 In this article, we theoretically analyzed the electrical  
 512 properties and suitability of FE/PE superlattices when used  
 513 as a gate material interfacing a *p*-type SC. We specifically  
 514 study a PZT/STO FE/PE superlattice sandwiched between  
 515 pSC and Pt electrodes. We calculate the electrical domain  
 516 structure as a function of repeating PZT/STO units and  
 517 provide numerical results of the overall polarization as a  
 518 function of temperature and the charge concentration  
 519 variation with gate voltage. Our results show that a MD  
 520 state inevitably forms in superlattices consisting of rela-  
 521 tively thick layers. This is in accordance with previous  
 522 studies [39, 54, 64, 66, 74]. We also find that superlattices  
 523 made up of relatively thinner layers may have a tendency



**Fig. 7** Flat-band energy diagrams along  $z$ -direction for 120 nm-thick pSC/PZT/STO heterostructure under **a** zero and **b** 0.8 V bias on STO. The thickness of PZT/STO superlattice stack is 105 nm with  $n = 7$  units. The highlighted region shows the pSC/superlattice interface that separates the pSC (left side) from the superlattice stack (right side)



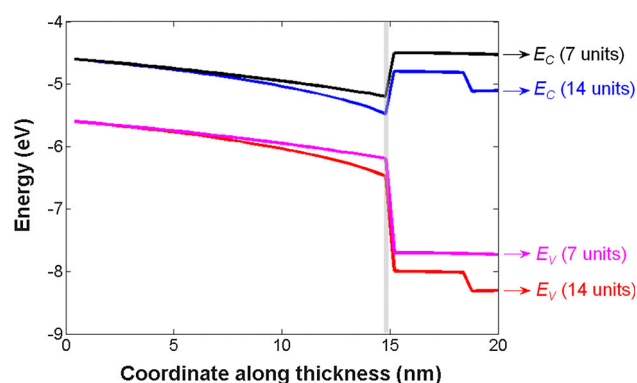
**Fig. 8** Flat-band energy diagrams along  $z$ -direction for 120-nm-thick pSC/PZT/STO heterostructure with **a** zero and **b** 0.8 V bias on STO. The thickness of PZT/STO superlattice stack is 105 nm with  $n = 14$  units. The highlighted region shows the pSC/superlattice interface that separates the pSC (left side) from the superlattice stack (right side)

524 to exist in a MD state that consists of domains with a  
525 relatively large domain periodicity. These thinner super-  
526 lattices may also be in a simple single-domain state but the  
527 formation of the monodomain state is accompanied by a  
528 reduction in the FE phase transformation temperature. Our  
529 calculations indicate that there is a significant difference  
530 between the electron density and the bias voltage for  
531 monodomain and MD superlattices. The stacks with thin-  
532 ner units display a more rapid bias-driven increase in  
533 electron density in the superlattice/pSC interface compared  
534 to the stacks with thicker repeating units. We explain this  
535 observation with the clearly different transition tempera-  
536 tures of the two stacks and different domain structures. The  
537 “softness” of the polarization in the stack with the lower  
538 transition temperature has a strong impact on the band

bending. Our findings indicate that FE superlattices in the  
MD state can potentially be used as gates in FET/MOS-  
FET-type architectures. The computations show that distinct  
on/off states of the SC channel are possible for gate  
bias voltages below 1 V.

We note that typically a high dielectric constant is  
required in the applications discussed herein—as gate  
materials enabling low power switching. However, in the  
off state, the gate itself should not store charge unless the  
gate is to act only as a switch and not a memory. Fur-  
thermore,  $D$  (or  $P$ )– $E$  hysteresis is another phenomena  
that would generate losses and should be avoided as well,  
and the MD state that forms in superlattices actually pro-  
vides the means to obtain non-hysteretic channel control.  
The materials systems we consider here could have a linear

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**Fig. 9** Flat-band energy diagrams along  $z$ -direction (from 0 to 20 nm) for 120-nm-thick pSC/PZT/STO heterostructure with  $n = 7$  and 14 units on STO at 0.8 V bias. The band banding near the pSC/superlattice interface (*highlighted region*) can clearly be seen for both heterostructures

554 large effective dielectric response but we do not expect  
555 hysteretic losses associated with total polarization switch-  
556 ing. Current leakage due to the presence of charged defects  
557 is another issue that factors into the device performance.  
558 The materials systems discussed here have excellent on/off  
559 switching properties and allow for additional functional-  
560 ities such as a tunable dielectric constant. Taking into  
561 account the additional parameters that factor into device  
562 design such as dielectric loss and leakage, a materials  
563 genomics type of optimization [75] could be useful to  
564 explore the full potential of FE superlattices in FET/  
565 MOSFET type of applications.

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570 **Compliance with ethical standards**

571 **Conflict of interest** The authors declare that they have no conflict  
572 of interest.

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